ADVANCED RECONSTRUCTION TECHNIQUES IN MRI - 1

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IMAGE RECONSTRUCTION IN MRI

The signal recorded in MRI is given by the Signal Equation,

 $s(t) = \int_{x} \int_{y} m(x, y) e^{-i2\pi [k_{x}(t)x + k_{y}(t)y]} dx dy \qquad \dots (1)$

This is basically a Fourier Transform of the image to be acquired m(x,y).

Hence a simple Inverse Fourier Transform would yield our required image.

• Magnetic Resonance Imaging is increasingly being used for fast imaging applications such as real-time cardiac imaging, functional brain imaging, etc.

• Imaging speed in MRI is mainly limited by different imaging parameters selected by the pulse sequences, the subject being imaged and the RF hardware system in operation.

• New pulse sequences have been developed in order to decrease the imaging time by a faster k-space scan.

• However, they may not be fast enough to facilitate imaging in real time.

• Thus, image reconstruction techniques have been developed, in order to enable faster acquisition in MRI.

Among these are,

a. Parallel Imaging Reconstruction

b. Partial Fourier Reconstruction

PARALLEL-IMAGING RECONSTRUCTION

WHAT IS PARALLEL-IMAGING?

• Parallel Imaging, is a technique, that uses phased array coils, for the purpose of faster scanning.

WHAT ARE PHASED ARRAY COILS?

• Phased array coils, as discovered by Roemer et al. in 1990, consist of a number of mutually decoupled surface coils that simultaneously receive MR signals.





• In parallel imaging, the spatial dependence of the B1 field of the receiver array coil is used to remove or prevent this aliasing.

• There are two basic methods used to avoid aliasing in Parallel Imaging. They are,

- 1. SENSE
- 2. SMASH









MATHEMATICAL EXPLANATION:

• In MRI, the reconstructed image is weighted by the component of receiver coil B_1 field that lies in the transverse plane and this fact is key to parallel imaging. For 2D imaging, I(x,y) is given by,

$$I(x,y) = B_1(x,y) M(x,y)$$
 ...(2)

where $B_1(x, y)$ is the component of the receive B_1 field that lies in the transverse magnetization, suitably defined to include relaxation, flow, diffusion, and transmit B_1 field nonuniformity effects.

• In the rotating frame, both M and B_1 appear static for onresonance spins. Both M and B_1 are represented by complex numbers. Introducing new subscripts that refer to each coil. Thus,

 $I_{i}(x,y) = C_{i}(x,y) M(x,y)$...(3)

where *C* is the coil B_1 field sensitivity and *j* refers to the *j*th coil.



• We take phase-encoded direction as y-direction in the image. We also drop the frequency-encoded direction.

• Let the total number of replicates due to aliasing at a pixel location y be N_A . N_A is pixel dependent and is determined by R and by the size and shape of the object.

• For an object with same diameter in the phase-encoded direction as the original FOV, $N_A = R$ everywhere.

• If the object diameter is smaller than L, then some pixels will have $N_A < R$.

• If the object diameter is larger than *L*, some pixels will have $N_A > R$ and there will be phase wrap even without the sense of FOV reduction.

• We can express the FOV reduction mathematically by saying that a *R*-fold FOV reduction results in a N_A -fold aliased image representation.

• For each location y, we can write the image signal $I_j(y)$ as a superposition of original object and displaced replicates.

$$I_{j}(y) = \sum_{n=0}^{N_{A}-1} C_{j}(y+nL/R) M(y+nL/R) ...(4)$$

where $j=0, 1, ..., N_C - 1$. N_C is the number of receive coils.

Depending on the location of y, the number of replicates can vary. If coil sensitivity, $C_j(y)$ can be measured, then for each value of y, then Eq. 4 would give us N_C simultaneous equations with N_A unknowns. The unknowns are aliased magnetization values M(y+nL/R). $I_j(y)$ is the reconstructed aliased image.





• If $N_C \ge N_A$, the equation can be inverted to find estimated transverse magnetization *M*. The most general solution that gives maximum image SNR is pseudoinverse.

$$M = [(C^{T}\psi^{-1}C)^{-1}C^{T}\psi^{-1}]I \qquad \dots (6)$$

where ψ is the $N_C X N_C$ noise correlation matrix where diagonal elements represent variance from a single coil and off-diagonal elements represent noise cross-correlation between two coils.

• If $N_C > N_A$, the inversion problem is over-determined. The extra degrees of freedom are used with noise correlation matrix to improve SNR.

• If $N_C = N_{A'}$ the coil noise correlation matrix drops out. This is because, *C* is square and thus its inverse exists. Thus, $(C^T \psi^{-1} C)^{-1} = C^{-1} \psi(C^T)^{-1}$. We get,

$$M = [(C^{\mathsf{T}}\psi^{-1}C)^{-1}C^{\mathsf{T}}\psi^{-1}]I = [C^{-1}\psi(C^{\mathsf{T}})^{-1}C^{\mathsf{T}}\psi^{-1}]I = C^{-1}I...(7)$$

• If in ψ the off diagonal elements are negligible and the diagonal elements are nearly equal to 1, ψ can be replaced by the Identity matrix. Thus,

$$M = [(C^{T}C)^{-1}C^{T}]I \qquad ...(8)$$

• Thus for coils that are well decoupled, there is no difference in SNR results if we use Eq. 8.

• For R=1 in SENSE, SNR is maximum. SENSE decreases the SNR as scan time is reduced. The SNR is given by,

$$SNR_{SENSE} = SNR_{NORMAL}$$
 ...(9)

g√R

where \sqrt{R} is the expected SNR loss that results from reducing scan time by a factor of *R*.

• The factor *g* is called geometric factor and represents noise magnification that occurs when aliasing is unwrapped. It is given by,

$$g_{i} = \sqrt{[(C^{T}\psi^{-1}C)^{-1}]_{ii}[(C^{T}\psi^{-1}C)]_{ii}} \qquad \dots (10)$$

where *i* refers to aliased pixel replicate number for the ith pixel and has range $0, 1, ..., N_A$ -1. Thus Eq. 10 gives geometry factor for all pixels.

• Thus, SNR is spatially dependent in SENSE.

• In general, g depends on the number of aliased replicates N_A and the coil sensitivity difference between aliased pixels.









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We drop the y subscript of k and introduce m as the measured phase-encoding line number. Thus the k-space data is

$$S_j(k_m) = \int C_j(y)M(y)e^{i2\pi k_m y}dy \qquad \dots (12)$$

where *j* refers to the coil number.

Suppose R=3, $S_j(k_m)$ is measured for m = 0, 3, 6 and so forth. Thus, for a given k-space line m, we wish to construct three new synthetic k-space lines:

$\hat{S}(k_m) = \int M(y) e^{i2\pi k m y} dy$	(13)
$S(\kappa_m) = \int M(y) e^{-2\pi i \pi y} dy$	(13)

 $\hat{S}(k_m + \Delta k) = \int M(y) e^{i2\pi k m y} e^{i2\pi \Delta k y} dy \qquad \dots (14)$

 $\hat{S}(k_m + 2\Delta k) = \int M(y) e^{i2\pi k_m y} e^{i2\pi (2\Delta k)y} dy \qquad \dots (15)$

where \hat{S} denotes the new k-space data.

The new k-space lines have no coil dependency and therefore no sensitivity weighting in the integrals on the right side.

The goal is to synthesize the additional complex exponentials $e^{i2\pi(p\Delta k)y}$ (where p=0,1,2) that appear in the integrals using coil sensitivity. If we can find the weighting factors that approximate the exponentials, the k-space can also be approximated. For example, let the coil weighting factors of $e^{i2\pi(p\Delta k)y}$ be $a_{j,p}$,

Nc-1

$$\sum_{j=0}^{\infty} a_{j,p} C_j(y) = e^{i2\pi(p\Delta k)y} \qquad (p=0,1,2,...R-1) \qquad ...(16)$$

We can obtain new k-space data,

 $\hat{S}(k_m + p\Delta k) = \int M(y) e^{i2\pi k_m y} e^{i2\pi (p\Delta k)y} dy \qquad \dots (17)$

which gives,

$$\hat{S}(k_m + p\Delta k) = \int M(y) e^{i2\pi k_m y} \sum_{j=0}^{Nc-1} a_{j,p} C_j(y) dy \qquad \dots (18)$$

Taking summation outside yields:

$$\hat{S}(k_m + p\Delta k) = \sum_{j=0}^{Nc-1} a_{j,p} \int C_j(y) \ M(y) e^{i2\pi k m y} \ dy \qquad \dots (19)$$

$$\hat{S}(k_m + p\Delta k) = \sum_{j=0}^{Nc-1} a_{j,p} S_j(k_m) \qquad ...(20)$$

This is the desired result. The unmeasured k-space lines without coil sensitivity weighting are constructed as a linear combination of the measured lines. New lines at the measured locations *m* are constructed the same way without coil sensitivity weighting. Coil weighting factor $a_{j,p}$ is independent of measured k-space line location k_m .













Direct Measurement can be carried out in two ways. In the first method, a separate calibration scan is acquired. In the second extra data is collected during the actual scan itself for calibration. In the second method, variable density sampling is used, such that lines near the center of k-space are sampled at Nyquist frequency to reconstruct a lowresolution sensitivity map.

Although direct measurement avoids the problem of patient motion, it results in longer scan time because of fully sampled calibration lines. To avoid this, the acceleration factor is increased while sampling the outer part of k-space.









ADVANTAGES OF PARALLEL IMAGING

- Considerable increase in imaging speed.
- High image SNR.

DISADVANTAGES OF PARALLEL IMAGING

• Although SNR is high, it decreases due to reduced scan time.



APPLICATIONS OF PARALLEL IMAGING

• SENSE is the most widespread used parallel MRI technique. It is used in

1. Contrast enhanced MR Angiography – SENSE enables higher spatial resolution at a constant scan time.

2. Cardiac imaging - the reduced scan time allows real-time cardiac imaging without breath-holding.



Figure 18. SENSE contrastenhanced MRA of the abdominal aorta with R=2. [1]

· GRAPPA is also clinically used. It is used in

1. Inhomogeneous regions, such as the lungs or abdomen where it can be difficult to determine spatial coil sensitivity information.

HOMEWORK #1

• Compare SMASH and SENSE techniques used in MRI.

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